



EUROPEAN UNION  
European Structural and Investment Funds  
Operational Programme Research,  
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# THE EFFECT OF MOISTURE ON SPECIFIC ENERGY DEMAND FOR KNIFE-MILLED WHEAT STRAW

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➤ Mechanical size reduction = **INITIAL STEP** of waste treatment technologies.

## ➤ WHY TO DO IT?

- + An increase of specific surface, bulk density.
- + Increasing efficiency of subsequent treatment.
- + Shearing or defibering of biomass particles.
- + Reduction in degree of polycrystallinity.
- + Easier handling, reducing transportation cost.

## ➤ SOME LIMITATIONS?

- High energy-demanded.
- Biomass behaviour.
- Technical limits of commercial size reduction machines.

| TECHNOLOGY                    | TARGETED PARTICLE SIZE |
|-------------------------------|------------------------|
| Pelleting<br>briquetting      | < 6 mm                 |
| Pulverized<br>combustion      | < 1 mm                 |
| Pyrolysis                     | 0.25-2.00 mm           |
| Fluid bed<br>gasification     | 0.12-10.00 mm          |
| Fermentation                  | 0.03-10 mm             |
| Lignocellulosic<br>distillery | 0.5-3.0 mm             |

MECHANICAL ENERGY NEED TO REDUCE PARTICLES FROM NATIVE/INITIAL  
TO A TARGETED PARTICLE SIZE BETWEEN MILL WORKING TOOLS

[1] Hendriks A.T.W.M., Zeeman G., 2009, Pretreatment to enhance the digestibility of lignocellulosic biomass, *Bioresource Technology*, 100, 10-18.

[2] Hoque M., Sokhansanj S., Naimi L., Bi X., Lim J., 2007, Review and analysis of performance and productivity of size reduction equipment for fibrous materials. ASABE Annual International Meeting, Minneapolis, Minnesota.

[3] Oyedeji O., Gitman P., Qu J., Webb E., 2020, Understanding the impact of lignocellulosic biomass variability on the size reduction process: A review, *Webb, ACS Sustainable Chemistry and Engineering*, 8, 2327-2343.

[4] Miao Z., Grift T.E., Hansen A.C., Ting K.C., 2011, Energy requirement for comminution of biomass in relation to particle physical properties, *Industrial Crops and Products*, 33, 504-513.

- Specific energy requirement listed **as single values**.
- **A little information** served regarding modelling of **energy demand on biomass characteristics**.
  - **regression curves** - power, exponential, polynomic or linear functions
  - **conventional models** - Bond, Rittinger, or Kick comminution laws

$$\frac{de}{dD} = -C \cdot D^{-r}$$

## AIMS:

1. To experimentally identify the effect of biomass characteristics (**flowrate, moisture, initial particle size**) and knife mill variables (**peripheral speed of the rotor, screen size**) on specific energy requirement.
2. To define and calibrate a model that allows predicting specific energy requirement for knife milling of wheat straw at different moistures.

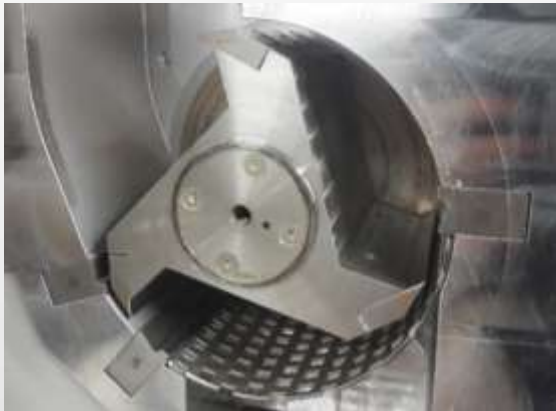


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# MATERIAL AND MACHINE

- Wheat straw with moistures 3.1 wt %, 8.1 wt %, 22.9 wt %
- the laboratory knife mill SM300 equipped with a three linear-bladed rotor
  - rotor speeds of  $10.2 \text{ m s}^{-1}$  (1500 rpm) and  $20.4 \text{ m s}^{-1}$  (3000 rpm)
  - screen sieves of openings 10 - 6 - 4 - 2 - 1 - 0.75 mm



- Each experimental run characterized by particle size characteristic before/after milling and by specific energy demand.

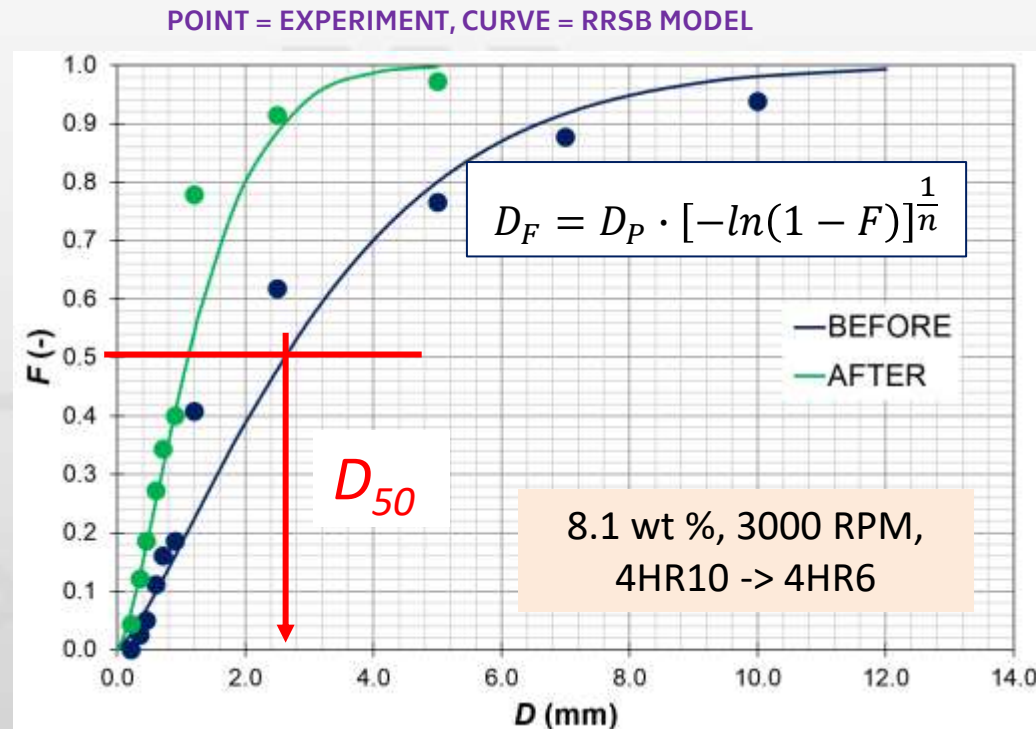
## Particle size characteristics:

- Screen sieve analysis by the ASABE standard S424.1.
- Applying RRSB model.
- Identifying  $D_{50}$  value.

## Specific energy demand:

- Analysing active power during milling and iddle state by power analyser in period 1 s.

$$e = \frac{1}{m} \cdot \left( \int_0^t P_{AM} dt - \int_0^t P_{AI} dt \right)$$



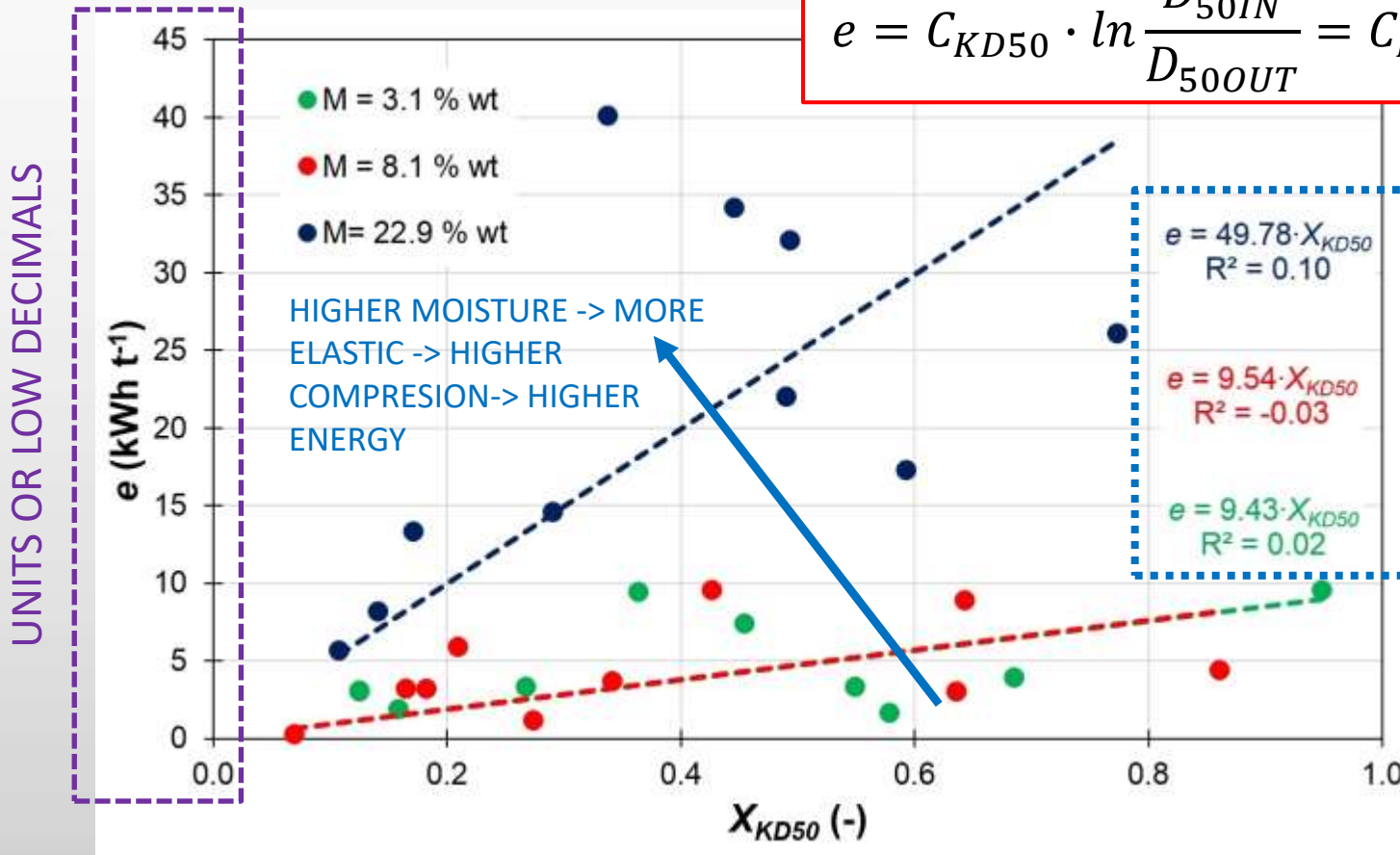
# RESULTS AND DISCUSSION

KICK THEORY:

- energy need to ensure a particle's elastic deformation followed by its crack

$$r=1 \quad \frac{de}{dD} = -C \cdot D^{-r}$$

$$e = C_{KD50} \cdot \ln \frac{D_{50IN}}{D_{50OUT}} = C_{KD50} \cdot X_{KD50}$$



POOR  
PRECISION



NOT  
APPLICABLE

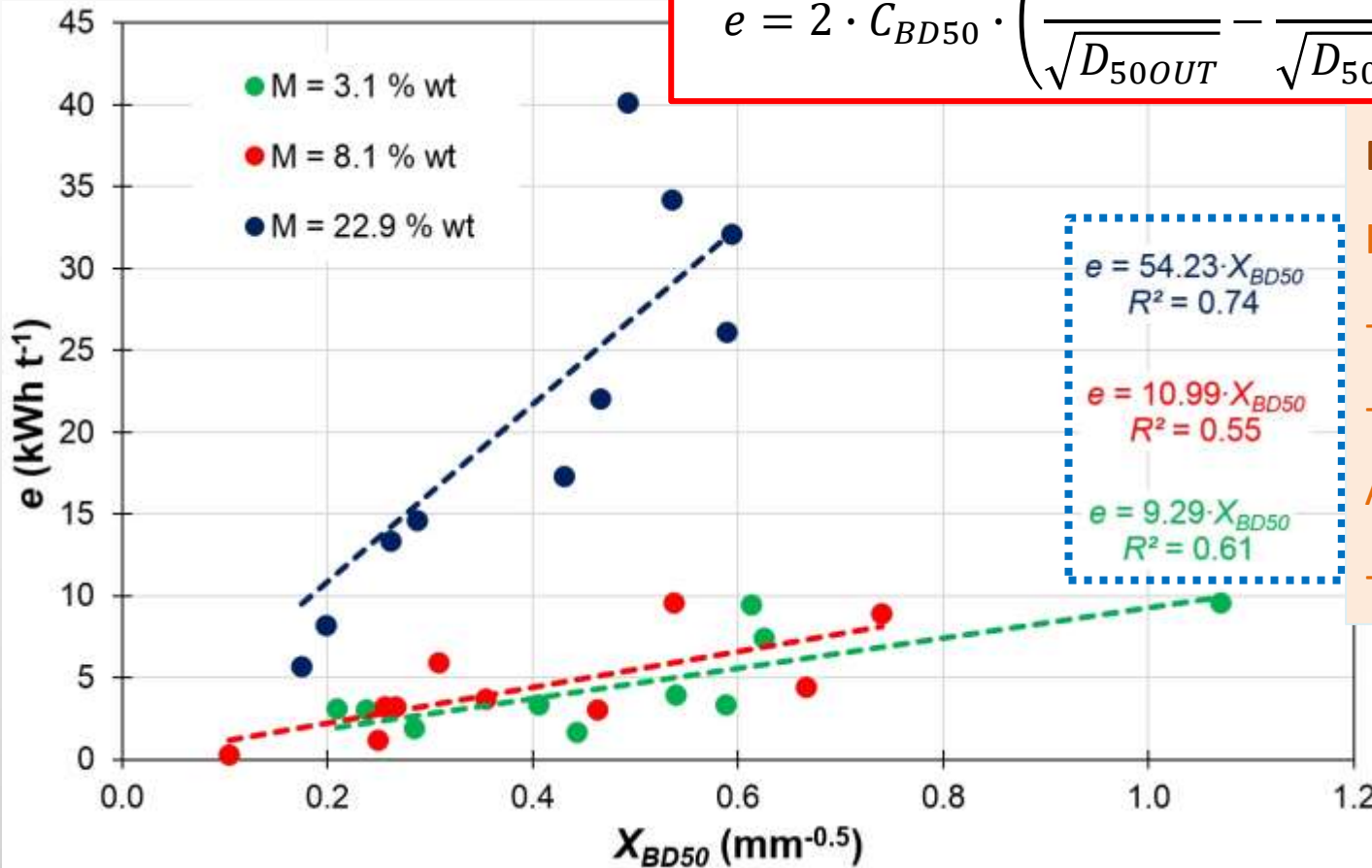
# RESULTS AND DISCUSSION

## BOND THEORY:

- energy needed for crack propagation is proportional to the new crack length

$$r=1.5 \quad \frac{de}{dD} = -C \cdot D^{-r}$$

$$e = 2 \cdot C_{BD50} \cdot \left( \frac{1}{\sqrt{D_{50OUT}}} - \frac{1}{\sqrt{D_{50IN}}} \right) = C_{BD50} \cdot X_{BD50}$$



$e = 54.23 \cdot X_{BD50}$   
 $R^2 = 0.74$   
 $e = 10.99 \cdot X_{BD50}$   
 $R^2 = 0.55$   
 $e = 9.29 \cdot X_{BD50}$   
 $R^2 = 0.61$

DRY STRAW = CUTTING  
 HIGHER MOISTURE  
 -> MORE ELASTIC  
 -> CUTTING, SHEARING  
 AND TEARING  
 -> HIGHER ENERGY

GOOD  
 PRECISION  
 APPLICABLE  
 ???

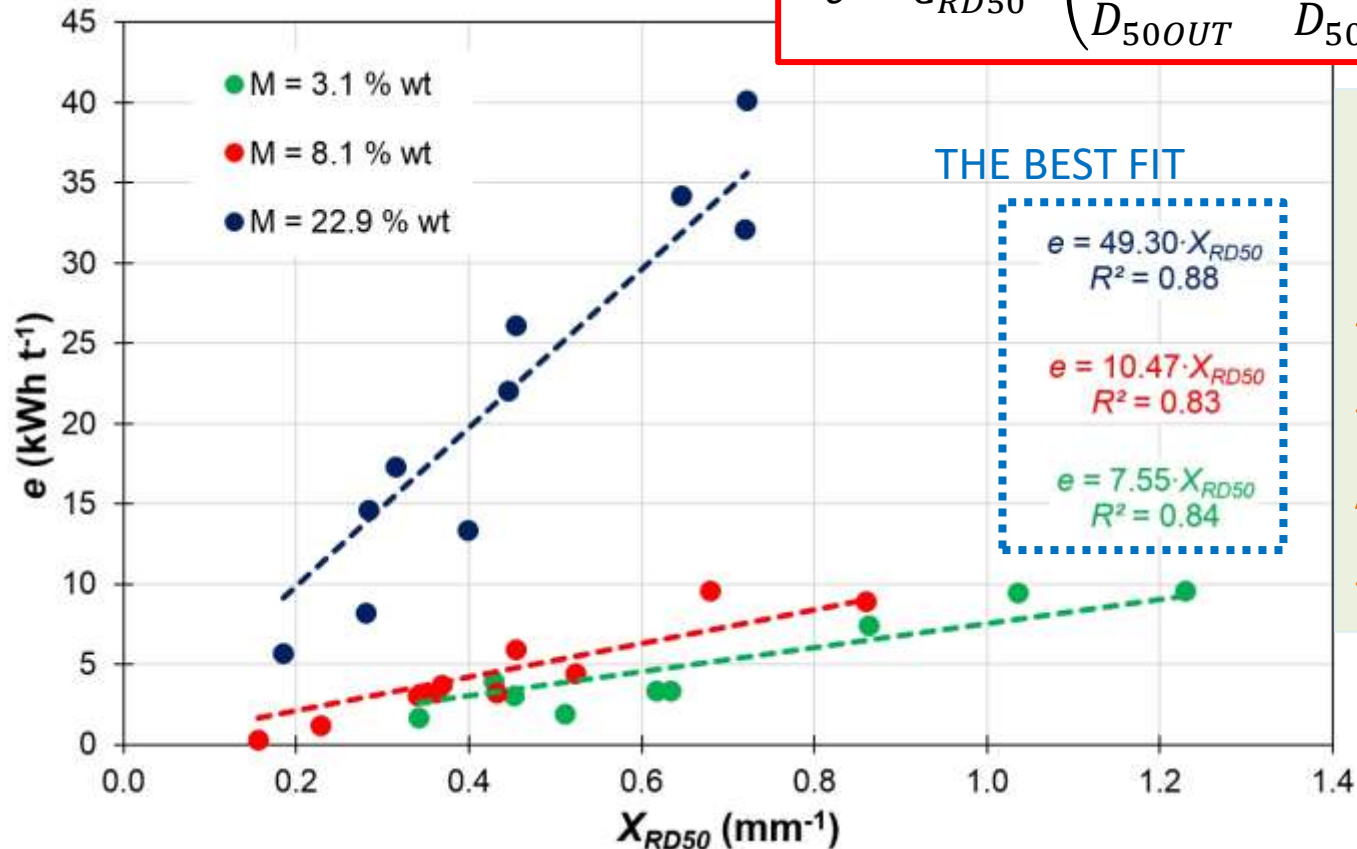


## RITTINGER THEORY:

- energy directly proportional to the particle surface increase

$$r=2 \quad \frac{de}{dD} = -C \cdot D^{-r}$$

$$e = C_{RD50} \cdot \left( \frac{1}{D_{50OUT}} - \frac{1}{D_{50IN}} \right) = C_{RD50} \cdot X_{RD50}$$



DRY STRAW = CUTTING  
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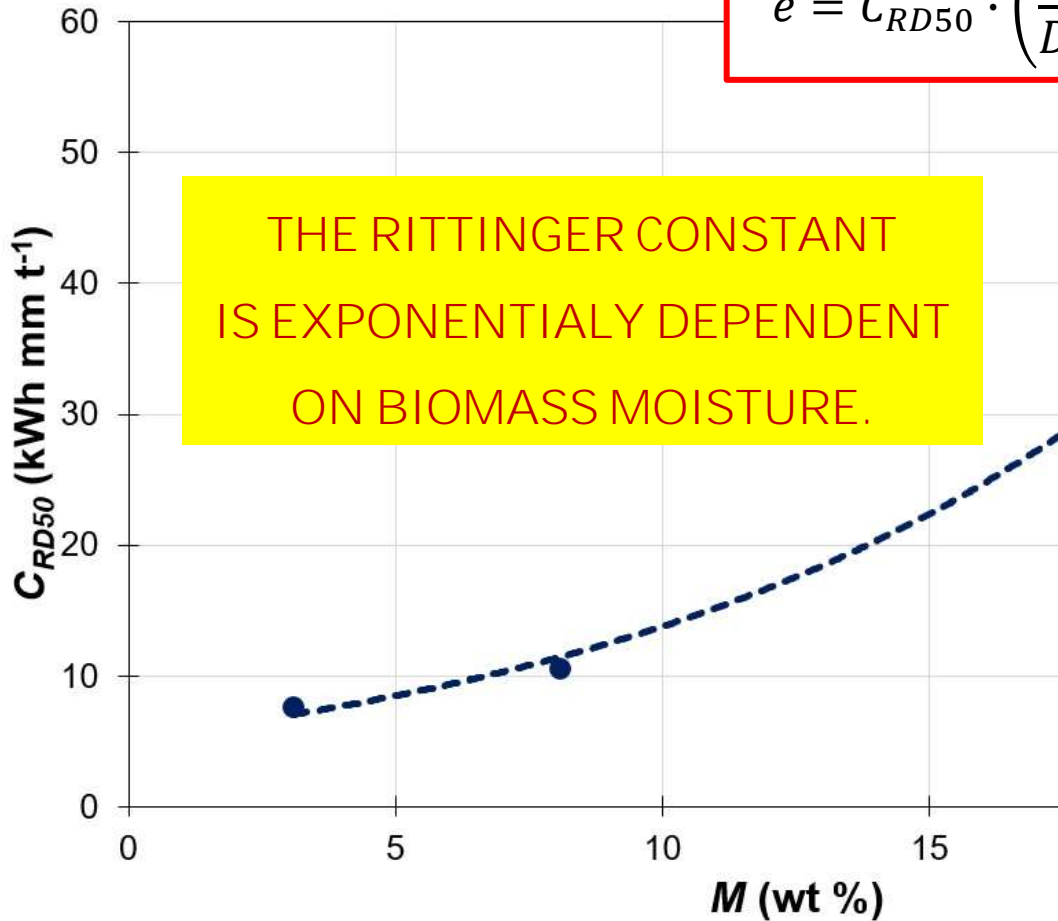


# RESULTS AND DISCUSSION

RITTINGER THEORY:

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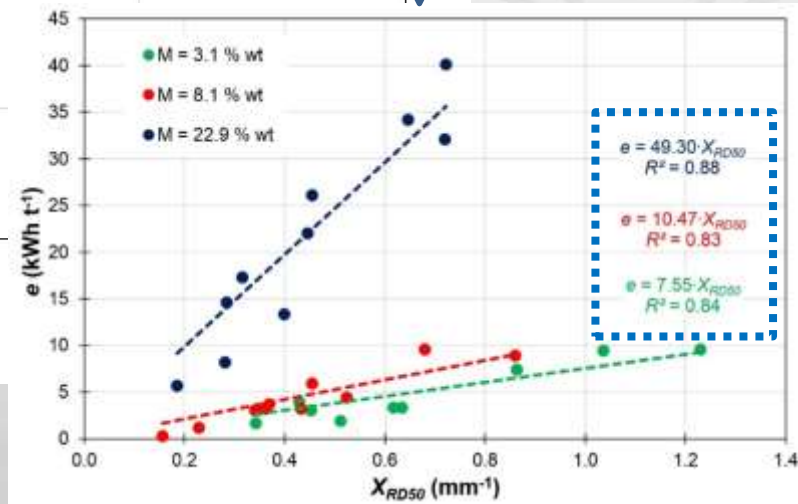
THE RITTINGER CONSTANT IS EXPONENTIALLY DEPENDENT ON BIOMASS MOISTURE.



$$C_{RD50} = 5.23e^{0.01 \cdot M}$$

$$R^2 = 0.99$$

EFFECT OF MOISTURE ???





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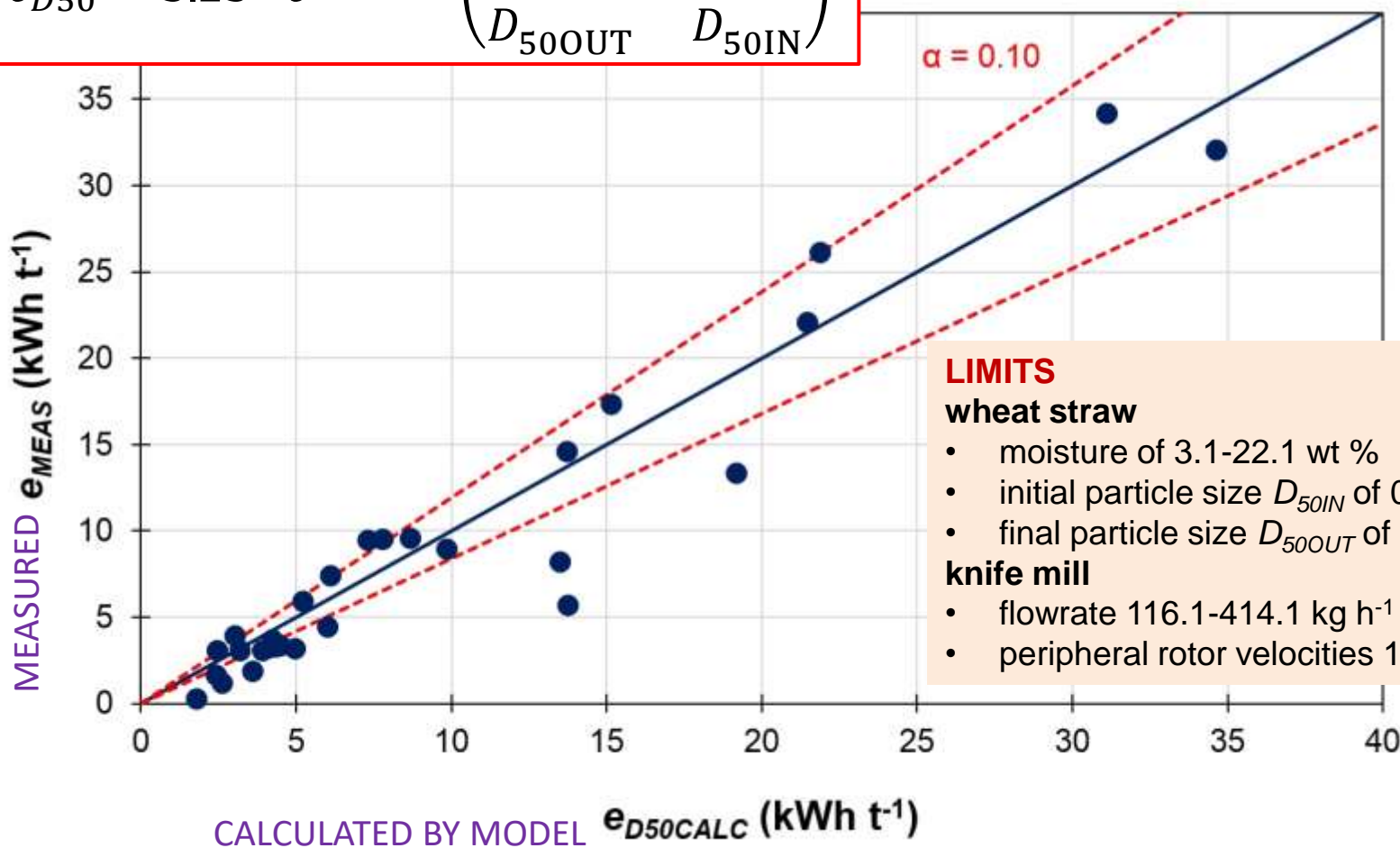
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# RESULTS AND DISCUSSION

DEFINING PREDICTION MODEL:

$$e_{D50} = 5.23 \cdot e^{0.01 \cdot M} \cdot \left( \frac{1}{D_{50OUT}} - \frac{1}{D_{50IN}} \right)$$

the precision expressed by the confidence intervals in the confidence level of  $\alpha = 0.1$





- The effect of moisture on specific energy demand for knife milled wheat straw experimentally quantified
- The specific energy requirement ranges in units or lower tents of kWh t<sup>-1</sup>.
- Comminution laws were tested to define mutual relations among specific energy demand, particle size characteristics and biomass moisture.

## MESSAGE TO TAKE HOME:

- The Rittinger comminution law showed the highest precision.
- The value of the Rittinger constant was power law dependent on moisture content.

$$e_{D50} = 5.23 \cdot e^{0.01 \cdot M} \cdot \left( \frac{1}{D_{50OUT}} - \frac{1}{D_{50IN}} \right)$$

### LIMITS

#### wheat straw

- moisture of 3.1-22.1 wt %
- initial particle size  $D_{50IN} = 0.29-2.61$  mm
- final particle size  $D_{50OUT} = 0.25 - 1.41$  mm

#### knife mill

- flowrate 116.1-414.1 kg h<sup>-1</sup> m<sup>-1</sup>
- peripheral rotor velocities 10.2-20.4 m s<sup>-1</sup>.



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# RESEARCH CENTRE OF LOW-CARBON ENERGY TECHNOLOGIES

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FACULTY OF MECHANICAL ENGINEERING  
Project reg. Nr. CZ.02.1.01/0.0/0.0/16\_019/0000753

The presentation and workshop were supported by the International Visegrad Fund under grant number 22120032 named "Green Deal strategies for V4 countries: The need and challenges to reach low-carbon industry".



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